

# **Analytic tomography of the mantle in a spherically Earth. The technique MZY**

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**Abstract.** An explicit expression for P-wave velocity is proposed to develop a novel tomographic technique in a spherically symmetric model of the Earth (MZY). The distribution of the P velocity structure in the mantle is determined using only 34 P- and 2 PcP- observed traveltimes. By applying a non-linear inversion, the P-residuals in the range between  $0^\circ$  and  $100^\circ$  are minimised up to a maximum value of 0.015 s. Furthermore, from the high quality computation of PcP traveltimes, with residuals much better than 0.13 s., it is possible to infer the existence of a brief low velocity layer in the D" region. This is then followed by a gradual increasing in the velocity profile towards the core, which begins at a depth of 2893.9 km.

**Key words:** D" shell, Earth's mantle, P-wave velocity, tomography, traveltimes.

## **Introduction**

To date, numerous studies use the arrival times of seismic waves to explore the Earth structure. Seismic arrival times have provided a fundamental constraint on the radial and lateral velocity structure of our planet. Sengupta and Toksoz (1976), Clayton and Comer (1983), Dziewonski (1984) among others, studied the variation of the P-wave velocity in the lower mantle. These works have been extended rapidly to the whole mantle (Pulliam et al., 1993) from many different viewpoints and perspectives, but concluding in almost all cases in interesting correlations with the structure predicted by the plate tectonics. On the other hand, reference models constitute the common basis for all the different studies concerning the Earth. Some of them are fairly relevant and well known in the seismological literature, as PREM (Dziewonski and Anderson, 1981), IASP91 (Kennet and Engdahl, 1991) and SP6 (Morelli and Dziewonski, 1993). They constitute the starting point for a number of applications, including seismic tomography and synthetic seismogram calculations. The strategy of finding an agreement between physical meaningful and

achieving observations is of crucial importance. A decreasing of the relative error between the reproduced and measured data becomes in an increasing knowledge of the main features concerning the Earth structure. In this sense, any effort made to improve the available reference models, will benefit on the current seismological knowledge, especially those concerning local deviations in boundary interfaces in the Earth's interior.

From this viewpoint, in this preliminary work we pretend to improve the fitting of reference traveltimes tables (JB: Jeffreys and Bullen, 1958; BSSA: Herrin et al., 1968) to observed traveltimes and, as consequence of that, to infer the slight deviations of the whole structure with respect to the average models. We have focused our attention on the tomography of the mantle, using and developing a non-linear inversion technique based on the analytical solution of the elliptical integrals involved in the theory of wave propagation. In this sense the approach described in this paper cannot be viewed like an empirical model. We demonstrate that the range of the achievement is large enough and, therefore, the real interpretation is to be an improvement for the reference model derived from the Herrin et al. traveltimes tables, used in this work. Eventually, this sort of agreement to respect the *observed* data (errors not larger than a particular threshold) has been imposed as a first objective of this study, but it is not unique. The use of an analytical function avoids the common strategy of deriving spherical averages from seismological observations via an inversion procedure (i.e., the least-square approach). An interesting comment of this performing can be found in Morelli and Dziewonski (1993). In our scheme, the inherent biased data distribution is largely overcome since only traveltimes tables are taking into account. This absence of real data is a major lack in the model we present in this paper, and we agree. However, we keep the opinion that the results should be interpreted in a different way as those derived from a reference model, because they maintain internal consistency and do not pretend to be an alternative to PREM, ISAP91 or SP6 models.

The use of analytical functions to derive a model that globally reproduces the observed traveltimes by acting locally on a multilayer and spherical mantle does not prescribe the meaning, from a physical viewpoint, of the new model. Indeed, the analytical tomography results in an improved understanding of some particular areas, for example the D'' layer at the base of the mantle. These features are the most relevant conclusions of our work as they provide some slight differences to the current knowledge of the mantle.

## Methodology

The trial P-wave velocity function used in this work to analyse the structure of the mantle can be summarised by the expression

$$v(r) = r \cdot (B - A \cdot \ln(r)) \quad , \quad (1)$$

where  $r$  is the radius, and  $(A,B)$  two independent parameters to be determined. This formula can be simplified by defining the function

$$w(r) = (B - A \cdot \ln(r)) \quad , \quad (2)$$

and then:

$$v(r) = r \cdot w(r) \quad . \quad (3)$$

The P-wave velocity function expressed in Eq. (1) has been used (Lana-Renault and Cid, 1991; Lana-Renault, 1998) to obtain different Earth models by varying the different parameters. The smoothness of this function makes it adequate to tomographic studies of the Earth's mantle, once a proper parameterisation is applied, i.e. a division in many spherical layers, which is the one followed in this work. Another useful property of the function described in Eq. (1) is that converts the elliptical integrals arisen during the hamiltonian formulation of ray propagation, into analytical functions. For example, for a ray crossing the first layer ( $i = 1$ ) of the mantle, who radius of the top surface is  $R_1$  (Earth's radius), the epicentral distance  $\Delta$  can be expressed as

$$\Delta = \frac{2 \cdot w_1}{A_1} \cdot \sinh\left(\frac{A_1 \cdot T}{2}\right) \quad , \quad (4)$$

where:

$$w_1 = w_1(R_1) = B_1 - A_1 \cdot \ln(R_1) \quad .$$

The general analytical expressions for  $\Delta$  and  $T$  can be obtained using the classical integral expressions (Bullen and Bolt, 1985)

$$\Delta = p \cdot \int_{r_p}^{r_o} r^{-1} \cdot \sqrt{\eta^2 - p^2} \, dr \quad , \quad (5)$$

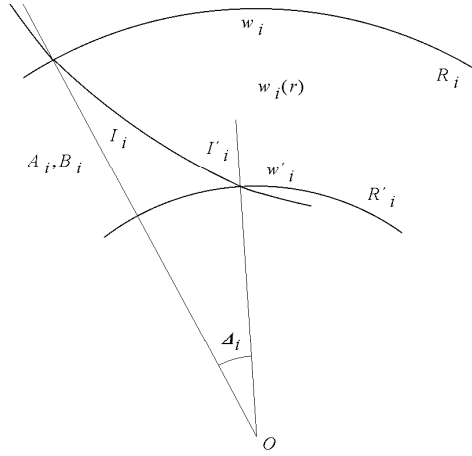
$$T = \int_{r_p}^{r_o} \eta^2 \cdot r^{-1} \cdot \sqrt{\eta^2 - p^2} \, dr \quad .$$

Denoting the angle of incidence at the top surface of the  $i^{th}$  layer by  $I_i$  and its radius by  $R_i$ , and similarly for the variables at the bottom ( $I_i'$  and  $R_i'$ ), see figure 1, it is always possible to write

$$w_i = w_i(R_i) = B_i - A_i \ln(R_i) = \frac{\text{sen}(I_i)}{p} \quad , \quad (6)$$

and

$$w'_i = w'_i(R'_i) = B_i - A_i \ln(R'_i) = \frac{\text{sen}(I'_i)}{p} \quad . \quad (7)$$



**Fig. 1.** P-trajectory traveling through a layer  $i$

In general, for a point  $P(r)$  we have

$$w_i(r) = B_i - A_i \ln(r) = \frac{\text{sen}(I)}{p} \quad . \quad (8)$$

Hence, through its derivative,

$$\frac{dr}{r \cdot \cos(I)} = -\frac{dI}{p \cdot A_i} \quad (9)$$

we can calculate the expressions (5) for a P-trajectory which travels from  $R_i$  to  $R'_i$

$$\Delta_i = \frac{\cos(I_i) - \cos(I'_i)}{p \cdot A_i} \quad , \quad (10)$$

$$T_i = \frac{1}{A_i} \cdot \ln \left[ \frac{\text{tg}\left(\frac{I'_i}{2}\right)}{\text{tg}\left(\frac{I_i}{2}\right)} \right] \quad . \quad (11)$$

Therefore, the observables at the Earth surface can be computed as a result of several additions of these computed values at each layer. That is, if one ray travels along  $k$  layers, the final epicentral distance and traveltimes are calculated through of the following  $2k+1$  equations:

$$\Delta = \frac{2}{p} \cdot \left( \sum_i \frac{\cos(I_i) - \cos(I'_i)}{A_i} + \frac{\cos(I_k)}{A_k} \right) , \quad (12)$$

$$T = 2 \cdot \left[ \sum_i \frac{1}{A_i} \cdot \ln \left[ \frac{\operatorname{tg}\left(\frac{I'_i}{2}\right)}{\operatorname{tg}\left(\frac{I_i}{2}\right)} \right] - \frac{1}{A_k} \cdot \ln \left( \operatorname{tg}\left(\frac{I_k}{2}\right) \right) \right] \quad (13)$$

and these  $2k-1$  auxiliary equations

$$p = \frac{\operatorname{sen}(I_i)}{w_i(R_i)} = \frac{\operatorname{sen}(I'_i)}{w_i(R'_i)} = \frac{\operatorname{sen}(I_k)}{w_k(R_k)} , \quad (14)$$

where:  $i = 1, 2, \dots, k-1$ .

On the other hand, the observables for a PcP-trajectory are calculated by the following  $2(k+1)$  equations:

$$\Delta = \frac{2}{p} \cdot \left( \sum_i \frac{\cos(I_i) - \cos(I'_i)}{A_i} \right) , \quad (15)$$

$$T = 2 \cdot \left[ \sum_i \frac{1}{A_i} \cdot \ln \left[ \frac{\operatorname{tg}\left(\frac{I'_i}{2}\right)}{\operatorname{tg}\left(\frac{I_i}{2}\right)} \right] \right] \quad (16)$$

and these  $2k$  auxiliary equations

$$p = \frac{\operatorname{sen}(I_i)}{w_i(R_i)} = \frac{\operatorname{sen}(I'_i)}{w_i(R'_i)} . \quad (17)$$

where:  $i = 1, 2, \dots, k$ .

Finally, by integrating Eq. (9) between  $P(R_i)$  and  $P(r)$ , it is easy to calculate the radius of any single point  $P(r)$  along the trajectory:

$$r = R_i \cdot \exp\left(\frac{\operatorname{sen}(I_i) - \operatorname{sen}(I)}{p \cdot A_i}\right) = R_i \cdot \exp\left(\frac{w_i - w_i(r)}{A_i}\right) . \quad (18)$$

## Results

With a single collection of observed traveltimes, it is possible to reproduce the observations on the Earth's surface for any event. For the sake of simplicity, as an example of the versatility and functionality of the proposed methodology, we have selected the datasets reproduced in *Herrin et al.* (1968). The sequence of calculations consists of determining the specific constants  $A_i$ ,  $w_i$  and  $w'_i$  ( $i = 1, \dots, N$ ), for each layer,  $N$  being the number of layers.

(Note that  $w'_i$  is a measure of the thickness of the  $i^{th}$  layer and that we don't use  $B_i$ . The parameter  $B_i$  is calculated after using the Eq. (6))

Let suppose these quantities are already known for the first  $k-1$  layers, except  $w'_{k-1}$ , the starting point for the  $k^{th}$  layer. The inverse problem can be posed as a system of non-linear equations (12-14) that will provide the parameters  $A_k$  and  $w_k$  of the layer  $k$ . We must use three P-observed trajectories reproducing three fixed points  $(\Delta_l, T_{ol}; l = 1, 2, 3)$  as boundary conditions for the system of  $3(2k+1)$  non linear equations with  $3(2k+1)$  unknowns  $(p_l, I_{ll}, I'_{ll}, I_{kl}, w'_{k-1}, w_k, A_k)$ . The solution is then iterated till assure a convergence criterion, in our case, a threshold for the computed residuals less than a certain value ( $10^{-15}$ ).

Known the values  $w'_{k-1}$ ,  $w_k$ , y  $A_k$ , we prove that the residual times  $T_o - T_c$  (observed minus computed time) of the all the others P-trajectories which also return to the surface-focus from the  $k^{th}$  layer are smaller than a determined  $\varepsilon$ . If it is not so, we begin again taking others three observables  $(\Delta_l, T_{ol})$  nearer among them.

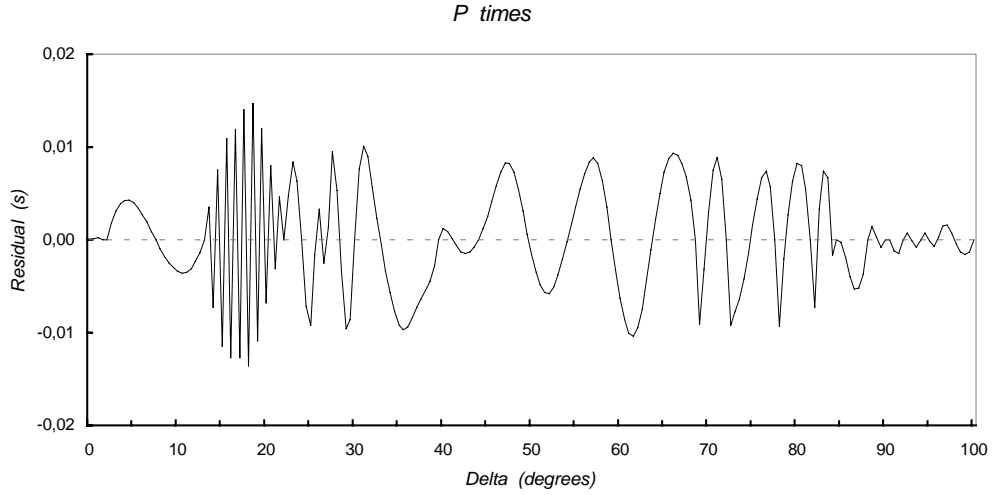
It is to be noted that the algebra applied in our methodology permits a discontinuity of the 1<sup>st</sup> kind ( $w'_{k-1} \neq w_k$ ) in the velocity function.

This last property can be analysed through the study of the derivative  $(dT/d\Delta)$  (*Herrin et al.*, 1968), in order to detect jumps in the selected velocity pattern. If we have the security that only a discontinuity of the 2<sup>nd</sup> kind ( $w'_{k-1} = w_k$ ) is present, then it is possible to work with only 2 observables  $(\Delta, T_o)$  or fixed boundary conditions, thus eliminating  $2k+1$  redundant equations from the global system.

In this case, the experience tells us that is much better to work with one observable  $(\Delta, T_o)$  and, thus, fixing the final of the  $k-1^{th}$  layer by a value for  $w'_{k-1}$ . and insuring that the residual times of all the P-trajectories which return from the  $k-1^{th}$  layer to the surface-focus are less than our  $\varepsilon$ . Thereby, we resolve a non linear system with only  $2k+1$  equations.

We have performed a complete description of the Mantle using a maximum residual time  $\varepsilon = 0.015$  s. and only 34 P-observed traveltimes. The total number of layers used in this description is 28. The last one finishes at a depth of 2810.1 km., maximum for the last P-observed trajectory at  $\Delta = 100^\circ$  according to *Herrin et al.* (1968), with  $T_o = 826.7303$  s. Once known the problematic of the lack of information for  $\Delta > 100^\circ$  and the special case of the D" shell, we have worked with

data available from  $\Delta > 88^\circ$  and maximum residuals of  $0.002$  s. See Table 1 and Residuals of P-travel times (Figure 2) for a graphic representation and further details.

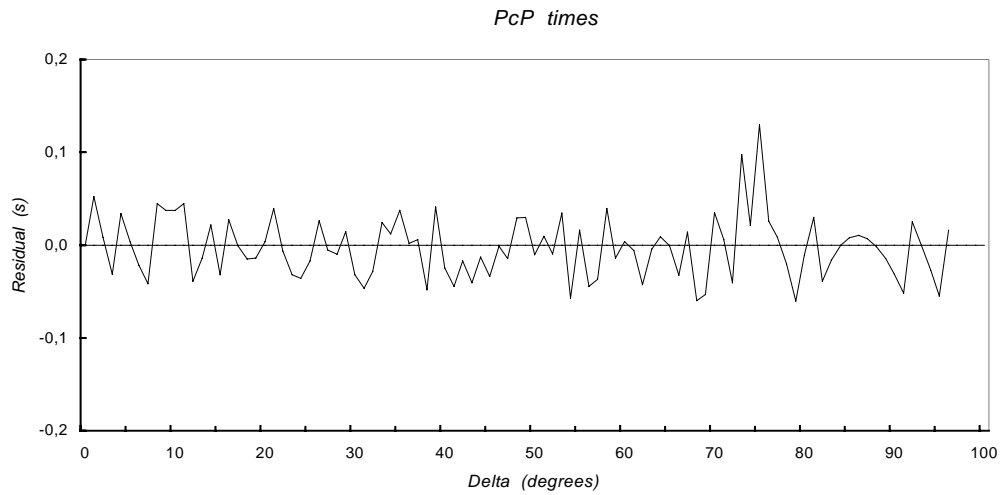


**Fig. 2.** P-residual times  $T_o - T_c$ .  $\Delta$ :  $0 - 100^\circ$  every  $0.5^\circ$ . Maximum residual  $0.015$  sec. at  $\Delta = 18.5^\circ$ .

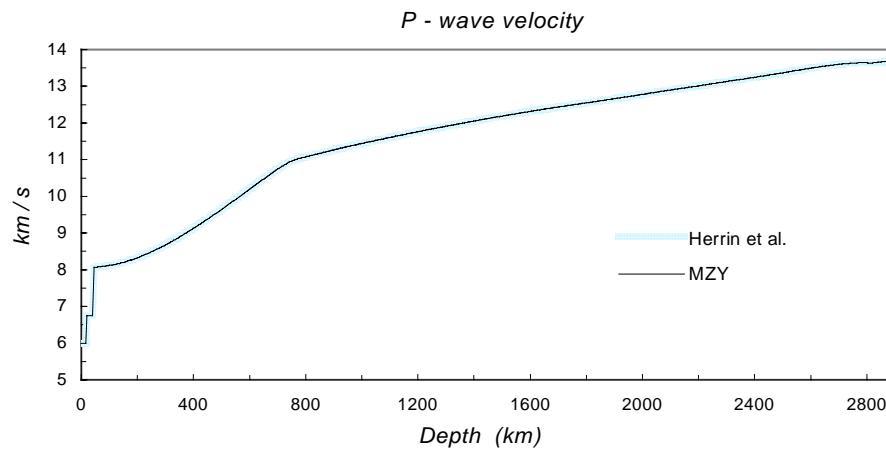
**The 29<sup>th</sup> layer.** Since the derivative associated with the surface-focus travel time ( $dT/d\Delta$ ) is effectively constant (Herrin *et al.*, 1968) beyond  $99.0^\circ$ , and that our residuals are practically zero for those points, we consider the boundary condition  $w'_{28} = 1/p(100^\circ) = w_{29}$  produces the best results. Thus, our problem is reduced to calculate the parameters  $w'_{29}$  (final layer) and  $A_{29}$ . For this purpose, we pose a non linear system with two PcP observables. One of these fixed points should always be the axial trajectory ( $\Delta = 0^\circ$ ;  $T_o = 511.3$  sec.) that allows us to use only one equation:

$$T = 2 \cdot \sum_i \frac{1}{A_i} \cdot \ln \left( \frac{w'_i}{w_i} \right) \quad (19)$$

We have considered that the other observable should be very separated from the first, and thus, selected  $\Delta = 93^\circ$ ;  $T_o = 795.2$  s as second observable. Once obtained the values  $w'_{29}$  and  $A_{29}$ , all the PcP residuals were balanced with an error less than  $0.13$  s. (Figure 3, Table 2 of PcP-travel times). By applying Eq. (18) we found the outer core at  $2893.9$  km. Further details can be seen in Figures 4, 5, 6 and Table 3 of P-wave velocity.



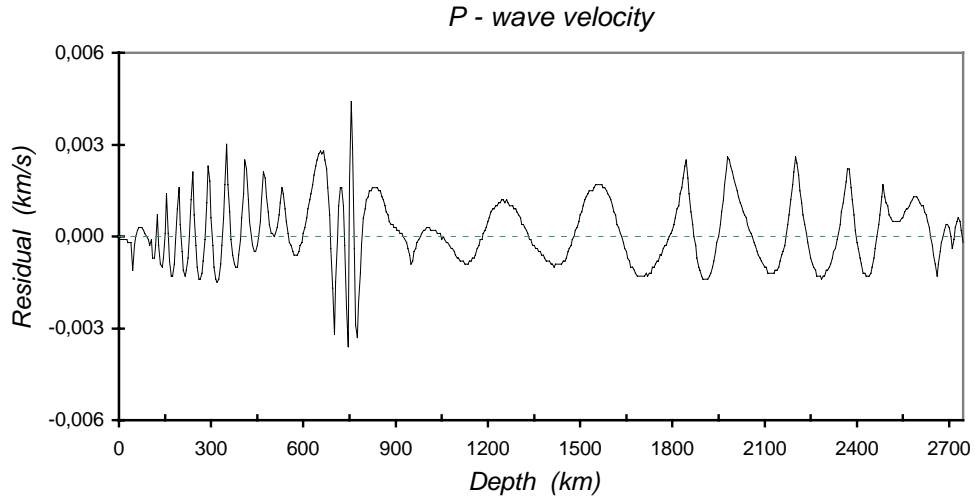
**Fig. 3.** PcP-residual times  $T_o - T_c$ .  $\Delta$ :  $0 - 96^\circ$  every  $1^\circ$ . Maximum residual  $0.13$  sec. at  $\Delta = 75^\circ$ . Depth Outer Core:  $2893.9$  km.



**Fig. 4.** P-wave velocity in the mantle. *Herrin et al.* versus *MZY*.

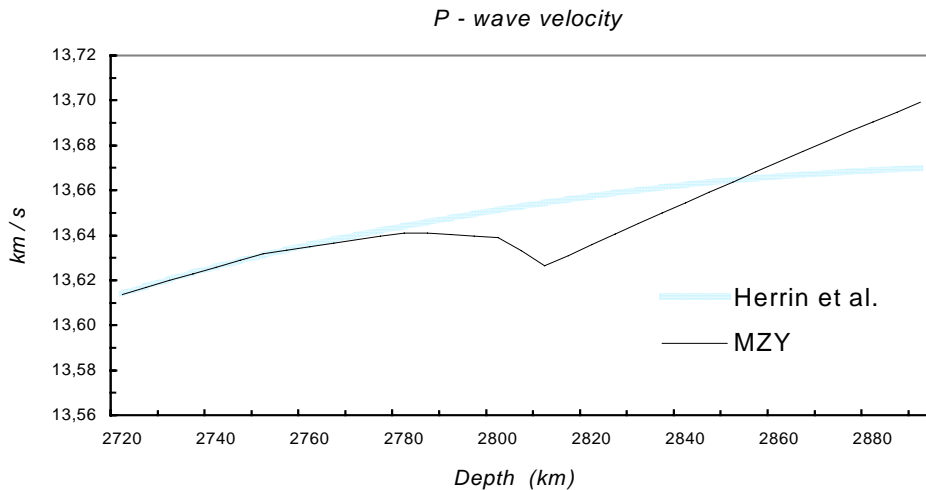
Fig. 4 shows a comparison between our velocity distribution and the one provided by *Herrin et al.* (1968). The most conspicuous difference is observed at  $2749.8$  km., final of the  $25^{th}$  layer, where the last trajectory returns to the surface at  $\Delta = 92^\circ$  and the corresponding residual is null. Figure 5 exhibits residuals of computed velocity *Herrin et al.* minus *MZY*. Let us note how the maximum residual is  $0.0044$  km/s at a depth of  $755$  km.





**Fig. 5.** Residual velocity *Herrin et al.* minus *MZY* in the mantle until a depth of 2745 km. Maximum residual: 0.0044 km/sec at a depth of 755 km.

From 2749.8 km. until the core-mantle boundary (*region D''*), our velocity distribution begins to be completely different to *Herrin et al.* (1968), as can be seen in Fig. 6. This is due that *Herrin et al.* adopted a special smooth velocity distribution to the region *D''* to explain the last results from *Taggart and Engdahl*, (1968), which indicated a slow increase of velocity towards the core. Morelli and Dziewonski (1993), in their SP6 model, obtained a continuous decrease from 2741 km. In our *MZY* model, we propose that *D''* region begins at 2780.7 km. with a brief (29.4 km.) negative gradient (layers number 27 and 28) followed by a slow increase until the core. With this profile we insure the residuals of all the observables P and PcP from *Herrin et al.* (1968) are minima, and reproduce accurately the observed times.



**Fig. 6.** P-wave velocity in *D''* region. *Herrin et al.* versus *MZY*

## **Concluding remarks**

We have presented a new technique to tomography the interior of the Earth for which one is able to obtain residual times less than a determined value  $\varepsilon$  for all observed trajectories P. The more minor is the value of  $\varepsilon$ , more genuine and real is the tomography.

Also, we have seen that the technique MZY developed is very easy to apply. Its potentiality is based in the function velocity found that it provides us analytical solutions for  $\Delta$  and T.

## **Acknowledgements**

The author is grateful to Dr. Javier Sabadell by the comments and suggestions made during the writing of the manuscript.

<b>Table 1</b>						<b>P travel times (sec.)</b>					p. 1/2
<b>La- yers</b>	$\Delta_{\text{initial}}$	$\Delta$	Observed	Computed	Residual	<b>La- yers</b>	$\Delta_{\text{initial}}$	$\Delta$	Observed	Computed	Residual
	$\Delta_{\text{final}}$		(Herrin & al. )	MZY	$T_o - T_c$		$\Delta_{\text{final}}$		(Herrin & al. )	MZY	$T_o - T_c$
<b>1</b>	0	0.00	0.0000	0.0000	0.0000	<b>15</b>	27.14	27.50	347.2025	347.1930	0.0095
		0.50	9.2663	9.2662	0.0001			28.00	351.6796	351.6743	0.0053
	7.85	1.00	18.5323	18.5321	0.0002			28.50	356.1456	356.1490	-0.0034
<b>2</b>	0.52	1.50	26.9525	26.9525	0.0000		29.00	360.6048	360.6144	-0.0096	
	10.66						29.50	365.0596	365.0682	-0.0086	
<b>3</b>	0.989	2.00	34.8630	34.8630	0.0000		30.00	369.5086	369.5086	0.0000	
		2.50	41.7231	41.7213	0.0018	<b>16</b>	30	30.50	373.9477	373.9401	0.0076
		3.00	48.5813	48.5782	0.0031			31.00	378.3751	378.3650	0.0101
		3.50	55.4373	55.4334	0.0039			31.50	382.7900	382.7810	0.0090
		4.00	62.2906	62.2864	0.0042			32.00	387.1923	387.1867	0.0056
		4.50	69.1410	69.1367	0.0043			32.50	391.5831	391.5808	0.0023
		5.00	75.9880	75.9840	0.0040			33.00	395.9621	395.9627	-0.0006
		5.50	82.8312	82.8278	0.0034			33.50	400.3281	400.3315	-0.0034
		6.00	89.6703	89.6676	0.0027			34.00	404.6807	404.6864	-0.0057
		6.50	96.5049	96.5030	0.0019			34.50	409.0193	409.0270	-0.0077
		7.00	103.3346	103.3337	0.0009			35.00	413.3435	413.3527	-0.0092
		7.50	110.1591	110.1591	0.0000			35.50	417.6532	417.6629	-0.0097
		8.00	116.9779	116.9789	-0.0010			36.00	421.9479	421.9573	-0.0094
		8.50	123.7908	123.7926	-0.0018			36.50	426.2269	426.2353	-0.0084
		9.00	130.5973	130.5998	-0.0025			37.00	430.4894	430.4967	-0.0073
		9.50	137.3970	137.4000	-0.0030			37.50	434.7347	434.7411	-0.0064
		10.00	144.1896	144.1930	-0.0034			38.00	438.9626	438.9681	-0.0055
		10.50	150.9747	150.9783	-0.0036			38.50	443.1730	443.1775	-0.0045
	11.00	157.7519	157.7554	-0.0035			39.00	447.3662	447.3690	-0.0028	
	11.50	164.5209	164.5240	-0.0031		39.5	39.50	451.5425	451.5425	0.0000	
	12.00	171.2813	171.2836	-0.0023		39.5	40.00	455.7020	455.7008	0.0012	
	12.50	178.0326	178.0340	-0.0014			40.50	459.8449	459.8440	0.0009	
	13.15	13.00	184.7746	184.7746	0.0000		41.00	463.9710	463.9709	0.0001	
<b>4</b>	13.15	13.50	191.4964	191.4929	0.0035		41.50	468.0802	468.0808	-0.0006	
	14.14	14.14	200.0582 *	200.0655	-0.0073		42.00	472.1723	472.1736	-0.0013	
<b>5</b>	14.14	14.50	204.8555	204.8480	0.0075		42.50	476.2473	476.2488	-0.0015	
	15.13	15.13	213.1831 *	213.1946	-0.0115		43.00	480.3051	480.3064	-0.0013	
<b>6</b>	15.13	15.50	218.0429	218.0320	0.0109		43.50	484.3454	484.3462	-0.0008	
	16.11	16.11	225.9644 *	225.9771	-0.0127		44.00	488.3680	488.3680	0.0000	
<b>7</b>	16.11	16.50	230.9845	230.9726	0.0119		44.50	492.3728	492.3716	0.0012	
	17.09	17.09	238.4697 *	238.4824	-0.0127		45.00	496.3596	496.3571	0.0025	
<b>8</b>	17.09	17.50	243.6096	243.5956	0.0140		45.50	500.3285	500.3244	0.0041	
	18.08	18.08	250.7491 *	250.7627	-0.0136		46.00	504.2791	504.2733	0.0058	
<b>9</b>	18.08	18.50	255.8408	255.8261	0.0147		46.50	508.2111	508.2038	0.0073	
	19.06	19.06	262.4864 *	262.4973	-0.0109		47.00	512.1242	512.1159	0.0083	
<b>10</b>	19.06	19.50	267.6136	267.6016	0.0120	<b>17</b>	47.50	516.0178	516.0096	0.0082	
	20.04	20.04	273.7653 *	273.7721	-0.0068			48.00	519.8920	519.8847	0.0073
<b>11</b>	20.04	20.50	278.9036	278.8956	0.0080			48.50	523.7469	523.7415	0.0054
	21.02	21.02	284.5832 *	284.5863	-0.0031			49.00	527.5828	527.5797	0.0031
<b>12</b>	21.02	21.50	289.7160	289.7114	0.0046			49.50	531.4001	531.3995	0.0006
	22	22.00	294.9501	294.9501	0.0000			50.00	535.1992	535.2008	-0.0016
<b>13</b>	22	22.50	300.0806	300.0759	0.0047			50.50	538.9802	538.9837	-0.0035
		23.00	305.1134	305.1050	0.0084			51.00	542.7433	542.7482	-0.0049
		23.50	310.0533	310.0470	0.0063			51.50	546.4887	546.4944	-0.0057
		24.00	314.9070	314.9070	0.0000			52.00	550.2164	550.2222	-0.0058
		24.50	319.6818	319.6890	-0.0072			52.50	553.9266	553.9317	-0.0051
	25.46	25.00	324.3869	324.3961	-0.0092			53.00	557.6192	557.6230	-0.0038
<b>14</b>	25.46	25.46	328.6614 *	328.6630	-0.0016		53.50	561.2941	561.2962	-0.0021	
		26.00	333.6295	333.6262	0.0033		54.00	564.9510	564.9512	-0.0002	
		26.50	338.1848	338.1873	-0.0025		54.50	568.5899	568.5882	0.0017	
	27.14	27.14	343.9656 *	343.9643	0.0013		55.00	572.2107	572.2072	0.0035	

Table 1						P travel times (sec.)					p. 2/2	
La- yers	$\Delta_{initial}$	$\Delta$	Observed (Herrin & al. )	Computed MZY	Residual $T_o - T_c$	La- yers	$\Delta_{initial}$	$\Delta$	Observed (Herrin & al. )	Computed MZY	Residual $T_o - T_c$	
17		55.50	575.8137	575.8082	0.0055	22	81.8	81.80	740.2336 *	740.2409	-0.0073	
		56.00	579.3986	579.3915	0.0071			82.50	82.50	743.9007	743.8974	0.0033
		56.50	582.9653	582.9569	0.0084			83.00	83.00	746.4926	746.4852	0.0074
		57.00	586.5135	586.5047	0.0088			83.50	83.50	749.0611	749.0544	0.0067
		57.50	590.0430	590.0348	0.0082			84.04	84.04	751.8075 *	751.8092	-0.0017
		58.00	593.5538	593.5475	0.0063			84.04	84.50	754.1271	754.1271	0.0000
	58.50	597.0462	597.0427	0.0035		85.00	85.00	756.6260	756.6263	-0.0003		
	59	59.00	600.5205	600.5205	0.0000		85.50	85.50	759.1042	759.1061	-0.0019	
	59	59.50	603.9770	603.9803	-0.0033		86.00	86.00	761.5636	761.5676	-0.0040	
		60.00	607.4162	607.4225	-0.0063		86.50	86.50	764.0064	764.0117	-0.0053	
		60.50	610.8385	610.8471	-0.0086		87.00	87.00	766.4338	766.4390	-0.0052	
		61.00	614.2444	614.2545	-0.0101		87.50	87.50	768.8465	768.8502	-0.0037	
		61.50	617.6343	617.6447	-0.0104		88	88.00	771.2455	771.2455	0.0000	
		62.00	621.0084	621.0179	-0.0095		88	88.50	773.6315	773.6301	0.0014	
		62.50	624.3668	624.3743	-0.0075		89	89.00	776.0056	776.0053	0.0003	
		63.00	627.7094	627.7138	-0.0044		89	89.50	778.3687	778.3695	-0.0008	
		63.50	631.0356	631.0367	-0.0011		90	90.00	780.7222	780.7222	0.0000	
		64.00	634.3452	634.3430	0.0022		90	90.50	783.0673	783.0673	0.0000	
		64.50	637.6379	637.6329	0.0050		91	91.00	785.4049	785.4061	-0.0012	
		65.00	640.9137	640.9064	0.0073		91	91.50	787.7356	787.7371	-0.0015	
		65.50	644.1724	644.1637	0.0087		92	92.00	790.0597	790.0597	0.0000	
		66.00	647.4142	647.4049	0.0093		92	92.50	792.3774	792.3767	0.0007	
		66.50	650.6392	650.6301	0.0091		93	93.00	794.6891	794.6892	-0.0001	
		67.00	653.8477	653.8395	0.0082		93	93.50	796.9953	796.9961	-0.0008	
		67.50	657.0398	657.0330	0.0068		94.03	94.03	799.4344 *	799.4344	0.0000	
		68.00	660.2151	660.2108	0.0043		94.03	94.50	801.5937	801.5930	0.0007	
		68.50	663.3731	663.3731	0.0000		95	95.00	803.8872	803.8873	-0.0001	
	69.08	69.08	667.0129 *	667.0220	-0.0091		95	95.50	806.1777	806.1784	-0.0007	
	69.08	69.50	669.6355	669.6387	-0.0032		96.123	96.123	809.0282 *	809.0279	0.0003	
		70.00	672.7383	672.7354	0.0029		96.123	96.50	810.7518	810.7503	0.0015	
		70.50	675.8202	675.8127	0.0075			97.00	813.0361	813.0345	0.0016	
		71.00	678.8805	678.8716	0.0089			97.50	815.3192	815.3185	0.0007	
		71.50	681.9193	681.9128	0.0065			98.00	817.6016	817.6021	-0.0005	
	72.35	72.00	684.9366	684.9366	0.0000			98.50	819.8838	819.8851	-0.0013	
	72.35	72.35	687.0340 *	687.0432	-0.0092			99.00	822.1660	822.1676	-0.0016	
		73.00	690.9092	690.9170	-0.0078			99.50	824.4481	824.4494	-0.0013	
		73.50	693.8665	693.8729	-0.0064		100	100.00	826.7303	826.7303	0.0000	
		74.00	696.8054	696.8096	-0.0042		100	99.5	824.4481	824.4498	-0.0017	
		74.50	699.7264	699.7279	-0.0015			99.0	822.1660	822.1694	-0.0034	
		75.00	702.6299	702.6283	0.0016			98.5	819.8838	819.8892	-0.0054	
		75.50	705.5159	705.5115	0.0044			98.0	817.6016	817.6094	-0.0078	
		76.00	708.3843	708.3776	0.0067			97.5	815.3192	815.3302	-0.0110	
		76.50	711.2346	711.2272	0.0074			97.0	813.0361	813.0520	-0.0159	
		77.00	714.0661	714.0604	0.0057			96.5	810.7518	810.7757	-0.0239	
	77.9	77.50	716.8776	716.8776	0.0000			96.0	808.4658	808.5028	-0.0370	
	77.9	77.90	719.1107 *	719.1200	-0.0093			95.618	806.7177 *	806.7715	-0.0538	
		78.50	722.4405	722.4426	-0.0021			96.0	808.4658	808.4805	-0.0147	
		79.00	725.1920	725.1893	0.0027		96.289	96.289	809.7871 *	809.7642	0.0229	
		79.50	727.9234	727.9171	0.0063				<i>interpolated *</i>			
		80.00	730.6349	730.6267	0.0082							
		80.50	733.3270	733.3190	0.0080							
		81.00	735.9998	735.9944	0.0054							
	81.8	81.50	738.6533	738.6533	0.0000							

Table 2 PcP travel times (sec.)							
$\Delta$	Observed (Herrin & al.)	Computed MZY	Residual $T_o - T_c$	$\Delta$	Observed (Herrin & al.)	Computed MZY	Residual $T_o - T_c$
0	511.3	511.300	0.00	49	611.9	611.870	0.03
1	511.4	511.348	0.05	50	615.5	615.511	-0.01
2	511.5	511.492	0.01	51	619.2	619.191	0.01
3	511.7	511.731	-0.03	52	622.9	622.910	-0.01
4	512.1	512.066	0.03	53	626.7	626.666	0.03
5	512.5	512.497	0.00	54	630.4	630.458	-0.06
6	513.0	513.022	-0.02	55	634.3	634.284	0.02
7	513.6	513.641	-0.04	56	638.1	638.144	-0.04
8	514.4	514.355	0.04	57	642.0	642.037	-0.04
9	515.2	515.163	0.04	58	646.0	645.961	0.04
10	516.1	516.063	0.04	59	649.9	649.914	-0.01
11	517.1	517.055	0.04	60	653.9	653.896	0.00
12	518.1	518.139	-0.04	61	657.9	657.906	-0.01
13	519.3	519.314	-0.01	62	661.9	661.943	-0.04
14	520.6	520.578	0.02	63	666.0	666.005	0.00
15	521.9	521.932	-0.03	64	670.1	670.091	0.01
16	523.4	523.373	0.03	65	674.2	674.201	0.00
17	524.9	524.901	0.00	66	678.3	678.333	-0.03
18	526.5	526.515	-0.01	67	682.5	682.486	0.01
19	528.2	528.214	-0.01	68	686.6	686.660	-0.06
20	530.0	529.996	0.00	69	690.8	690.853	-0.05
21	531.9	531.861	0.04	70	695.1	695.065	0.04
22	533.8	533.806	-0.01	71	699.3	699.294	0.01
23	535.8	535.832	-0.03	72	703.5	703.540	-0.04
24	537.9	537.936	-0.04	73	707.9	707.802	0.10
25	540.1	540.117	-0.02	74	712.1	712.079	0.02
26	542.4	542.374	0.03	75	716.5	716.370	0.13
27	544.7	544.705	-0.01	76	720.7	720.675	0.03
28	547.1	547.110	-0.01	77	725.0	724.992	0.01
29	549.6	549.586	0.01	78	729.3	729.320	-0.02
30	552.1	552.132	-0.03	79	733.6	733.660	-0.06
31	554.7	554.747	-0.05	80	738.0	738.010	-0.01
32	557.4	557.428	-0.03	81	742.4	742.370	0.03
33	560.2	560.176	0.02	82	746.7	746.739	-0.04
34	563.0	562.988	0.01	83	751.1	751.116	-0.02
35	565.9	565.863	0.04	84	755.5	755.500	0.00
36	568.8	568.798	0.00	85	759.9	759.892	0.01
37	571.8	571.794	0.01	86	764.3	764.290	0.01
38	574.8	574.848	-0.05	87	768.7	768.693	0.01
39	578.0	577.959	0.04	88	773.1	773.102	0.00
40	581.1	581.125	-0.02	89	777.5	777.515	-0.01
41	584.3	584.345	-0.04	90	781.9	781.932	-0.03
42	587.6	587.617	-0.02	91	786.3	786.352	-0.05
43	590.9	590.940	-0.04	92	790.8	790.775	0.03
44	594.3	594.313	-0.01	93	795.2	795.200	0.00
45	597.7	597.734	-0.03	94	799.6	799.627	-0.03
46	601.2	601.202	0.00	95	804.0	804.055	-0.05
47	604.7	604.714	-0.01	96	808.5	808.484	0.02
48	608.3	608.271	0.03	96.289		809.764	

**Table 3**

Data MZY		Depth (km)	P-wave velocity (km/s)			Data MZY		p. 1/4	P-wave velocity (km/s)		
Radius (km)	$v_i$ (km/s)		Herrin & al.	MZY	Residual	Radius (km)	$v_i$ (km/s)		Herrin & al.	MZY	Residual
			Radius of surface-focus = 6371.028						Radius of surface-focus = 6371.028		
<b>Layers</b>	$B_i$ ( $\times 10^{-2}$ )					<b>Layers</b>	$B_i$ ( $\times 10^{-2}$ )				
	$A_i$ ( $\times 10^{-3}$ )						$A_i$ ( $\times 10^{-3}$ )				
Depth (km)	$v'_i$ (km/s)			H. & al. - MZY		Depth (km)	$v'_i$ (km/s)		H. & al. - MZY		
6371.028	6.0000	0	6.0000	6.0001	-0.0001	6021.290062	8.8862	350	8.8905	8.8875	0.0030
1	0.92341045	5	6.0000	6.0001	-0.0001			355	8.9131	8.9114	0.0017
	0.94666548	10	6.0000	6.0001	-0.0001			360	8.9360	8.9352	0.0008
15.001533	6.0001	15	6.0000	6.0001	-0.0001			365	8.9590	8.9591	-0.0001
6356.026467	6.7500	20	6.7500	6.7501	-0.0001			370	8.9823	8.9829	-0.0006
2	1.04491768	25	6.7500	6.7501	-0.0001	10	5.59329351	375	9.0058	9.0067	-0.0009
	1.07194400	30	6.7500	6.7502	-0.0002		6.25724227	380	9.0294	9.0304	-0.0010
		35	6.7500	6.7502	-0.0002			385	9.0532	9.0542	-0.0010
40.053935	6.7502	40	6.7500	6.7502	-0.0002			390	9.0773	9.0779	-0.0006
6330.974065	8.0540	45	8.0582	8.0593	-0.0011			395	9.1015	9.1016	-0.0001
		50	8.0642	8.0645	-0.0003			400	9.1258	9.1252	0.0006
		55	8.0698	8.0698	0.0000			405	9.1503	9.1489	0.0014
		60	8.0753	8.0751	0.0002	411.322422	9.1787	410	9.1750	9.1725	0.0025
		65	8.0806	8.0803	0.0003	5959.705578	9.1787	415	9.1999	9.1977	0.0022
	2.16670136	70	8.0859	8.0856	0.0003			420	9.2248	9.2236	0.0012
	2.32998530	75	8.0911	8.0908	0.0003			425	9.2499	9.2494	0.0005
		80	8.0962	8.0960	0.0002			430	9.2752	9.2752	0.0000
		85	8.1013	8.1012	0.0001			435	9.3007	9.3010	-0.0003
		90	8.1064	8.1064	0.0000			440	9.3262	9.3267	-0.0005
		95	8.1115	8.1116	-0.0001	11	5.99325871	445	9.3519	9.3524	-0.0005
104.957687	8.1219	100	8.1165	8.1168	-0.0003		6.71735442	450	9.3778	9.3781	-0.0003
6266.070313	8.1219	105	8.1219	8.1220	-0.0001			455	9.4038	9.4038	0.0000
4	2.51841026	110	8.1285	8.1292	-0.0007			460	9.4299	9.4294	0.0005
	2.73226453	115	8.1356	8.1363	-0.0007			465	9.4562	9.4550	0.0012
		120	8.1432	8.1435	-0.0003			470	9.4826	9.4805	0.0021
125.320	8.1511	125	8.1513	8.1506	0.0007	472.071820	9.4911	475	9.5091	9.5072	0.0019
6245.707939	8.1511	130	8.1599	8.1602	-0.0003	5898.956180	9.4911	480	9.5358	9.5345	0.0013
		135	8.1690	8.1699	-0.0009			485	9.5626	9.5618	0.0008
	2.97405843	140	8.1786	8.1796	-0.0010			490	9.5895	9.5891	0.0004
	3.25362200	145	8.1886	8.1893	-0.0007			495	9.6165	9.6164	0.0001
		150	8.1991	8.1990	0.0001	12	6.31396167	500	9.6437	9.6436	0.0001
155.027311	8.2087	155	8.2101	8.2087	0.0014		7.08672019	505	9.6709	9.6709	0.0000
6216.000689	8.2087	160	8.2214	8.2213	0.0001			510	9.6981	9.6980	0.0001
		165	8.2332	8.2340	-0.0008			515	9.7255	9.7252	0.0003
	3.50244082	170	8.2454	8.2467	-0.0013			520	9.7530	9.7523	0.0007
	3.85853274	175	8.2580	8.2593	-0.0013			525	9.7805	9.7794	0.0011
		180	8.2710	8.2719	-0.0009	531.559687	9.8149	530	9.8080	9.8064	0.0016
		185	8.2843	8.2845	-0.0002	5839.468313	9.8149	535	9.8356	9.8342	0.0014
193.795314	8.3067	190	8.2980	8.2971	0.0009			540	9.8632	9.8623	0.0009
6177.232686	8.3067	195	8.3120	8.3104	0.0016			545	9.8908	9.8903	0.0005
		200	8.3264	8.3260	0.0004			550	9.9185	9.9184	0.0001
		205	8.3410	8.3415	-0.0005			555	9.9462	9.9464	-0.0002
	4.03019188	210	8.3560	8.3571	-0.0011			560	9.9740	9.9743	-0.0003
	4.46315376	215	8.3713	8.3726	-0.0013			565	10.0018	10.0023	-0.0005
		220	8.3870	8.3881	-0.0011			570	10.0296	10.0302	-0.0006
		225	8.4029	8.4036	-0.0007			575	10.0574	10.0580	-0.0006
239.227039	8.4476	230	8.4191	8.4191	0.0000			580	10.0853	10.0859	-0.0006
6131.800961	8.4476	235	8.4357	8.4345	0.0012			585	10.1132	10.1137	-0.0005
		240	8.4525	8.4504	0.0021			590	10.1411	10.1414	-0.0003
		245	8.4696	8.4689	0.0007			595	10.1690	10.1692	-0.0002
		250	8.4870	8.4873	-0.0003			600	10.1970	10.1969	0.0001
	4.55770255	255	8.5047	8.5057	-0.0010			605	10.2249	10.2246	0.0003
	5.06801092	260	8.5227	8.5241	-0.0014	13	6.50401417	610	10.2528	10.2522	0.0006
		265	8.5410	8.5424	-0.0014		7.30586668	615	10.2807	10.2798	0.0009
		270	8.5595	8.5607	-0.0012			620	10.3086	10.3074	0.0012
		275	8.5783	8.5791	-0.0008			625	10.3364	10.3350	0.0014
		280	8.5973	8.5974	-0.0001			630	10.3642	10.3625	0.0017
		285	8.6167	8.6156	0.0011			635	10.3920	10.3900	0.0020
291.392218	8.6390	290	8.6362	8.6339	0.0023			640	10.4197	10.4174	0.0023
6079.635782	8.6390	295	8.6561	8.6543	0.0018			645	10.4474	10.4449	0.0025
		300	8.6762	8.6756	0.0006			650	10.4750	10.4723	0.0027
		305	8.6966	8.6969	-0.0003			655	10.5024	10.4996	0.0028
		310	8.7172	8.7182	-0.0010			660	10.5297	10.5270	0.0027
	5.09632938	315	8.7380	8.7394	-0.0014			665	10.5570	10.5542	0.0028
	5.68621977	320	8.7591	8.7606	-0.0015			670	10.5840	10.5815	0.0025
		325	8.7804	8.7818	-0.0014			675	10.6109	10.6087	0.0022
		330	8.8020	8.8029	-0.0009			680	10.6375	10.6359	0.0016
		335	8.8238	8.8241	-0.0003			685	10.6638	10.6631	0.0007
		340	8.8458	8.8452	0.0006			690	10.6899	10.6903	-0.0004
349.737938	8.8862	345	8.8680	8.8663	0.0017			695	10.7157	10.7174	-0.0017
						700.177664	10.7454	700	10.7412	10.7444	-0.0032

**Table 3**

Data MZY		Depth (km)	P-wave velocity (km/s)			Data MZY		p. 2/4	P-wave velocity (km/s)			
Radius (km)	$V_i$ (km/s)		Radius of surface-focus = 6371.028			Radius (km)	$V_i$ (km/s)		Depth (km)	Herrin & al.	MZY	Residual H. & al. - MZY
Layers	$B_i$ ( $\times 10^{-2}$ )		Herrin & al.	MZY	Residual H. & al. - MZY	Layers	$B_i$ ( $\times 10^{-2}$ )					
	$A_i$ ( $\times 10^{-3}$ )					$A_i$ ( $\times 10^{-3}$ )						
	$V_i$ (km/s)					$V_i$ (km/s)						
5670.850336	10.7454	705	10.7664	10.7679	-0.0015			1115	11.6288	11.6296	-0.0008	
14	5.85891401 6.55949029	710	10.7911	10.7912	-0.0001			1120	11.6367	11.6375	-0.0008	
		715	10.8154	10.8144	0.0010			1125	11.6446	11.6455	-0.0009	
		720	10.8392	10.8376	0.0016			1130	11.6525	11.6534	-0.0009	
		725	10.8624	10.8608	0.0016			1135	11.6604	11.6613	-0.0009	
		730	10.8850	10.8840	0.0010			1140	11.6684	11.6692	-0.0008	
		735	10.9068	10.9071	-0.0003			1145	11.6763	11.6771	-0.0008	
		740	10.9279	10.9302	-0.0023			1150	11.6842	11.6849	-0.0007	
5626.918216	10.9492	745	10.9479	10.9515	-0.0036			1155	11.6921	11.6928	-0.0007	
15	4.12047826 4.54632080	750	10.9663	10.9645	0.0018			1160	11.7000	11.7006	-0.0006	
		755	10.9819	10.9775	0.0044			1165	11.7080	11.7084	-0.0004	
		760	10.9933	10.9904	0.0029			1170	11.7159	11.7162	-0.0003	
		765	11.0029	11.0033	-0.0004			1175	11.7238	11.7239	-0.0001	
		770	11.0134	11.0163	-0.0029			1180	11.7316	11.7317	-0.0001	
		775	11.0240	11.0273	-0.0033			1185	11.7395	11.7394	0.0001	
		780	11.0348	11.0370	-0.0022			1190	11.7473	11.7471	0.0002	
16	3.57557893 3.91494425	785	11.0455	11.0467	-0.0012			1195	11.7551	11.7548	0.0003	
		790	11.0561	11.0564	-0.0003			1200	11.7629	11.7624	0.0005	
		795	11.0666	11.0660	0.0006			1205	11.7707	11.7701	0.0006	
		800	11.0766	11.0757	0.0009			1210	11.7785	11.7777	0.0008	
		805	11.0865	11.0853	0.0012			1215	11.7862	11.7853	0.0009	
		810	11.0962	11.0949	0.0013			1220	11.7938	11.7929	0.0009	
		815	11.1060	11.1045	0.0015			1225	11.8015	11.8005	0.0010	
		820	11.1156	11.1141	0.0015			1230	11.8091	11.8081	0.0010	
		825	11.1252	11.1236	0.0016			1235	11.8167	11.8156	0.0011	
		830	11.1348	11.1332	0.0016			1240	11.8242	11.8231	0.0011	
		835	11.1443	11.1427	0.0016			1245	11.8318	11.8306	0.0012	
		840	11.1538	11.1522	0.0016			1250	11.8393	11.8381	0.0012	
		845	11.1632	11.1617	0.0015			1255	11.8467	11.8456	0.0011	
		850	11.1726	11.1711	0.0015			1260	11.8542	11.8530	0.0012	
		855	11.1819	11.1806	0.0013			1265	11.8616	11.8605	0.0011	
		860	11.1912	11.1900	0.0012			1270	11.8689	11.8679	0.0010	
		865	11.2004	11.1994	0.0010			1275	11.8763	11.8753	0.0010	
		870	11.2096	11.2088	0.0008			1280	11.8836	11.8826	0.0010	
		875	11.2189	11.2182	0.0007			1285	11.8909	11.8900	0.0009	
		880	11.2281	11.2276	0.0005			1290	11.8982	11.8973	0.0009	
		885	11.2373	11.2369	0.0004			1295	11.9054	11.9046	0.0008	
		890	11.2466	11.2462	0.0004		17	3.48245516	1300	11.9126	11.9119	0.0007
		895	11.2558	11.2555	0.0003		3.80663410	1305	11.9198	11.9192	0.0006	
900	11.2651	11.2648	0.0003			1310	11.9269	11.9265	0.0004			
905	11.2743	11.2741	0.0002			1315	11.9341	11.9337	0.0004			
910	11.2835	11.2833	0.0002			1320	11.9412	11.9409	0.0003			
915	11.2927	11.2926	0.0001			1325	11.9483	11.9481	0.0002			
920	11.3019	11.3018	0.0001			1330	11.9554	11.9553	0.0001			
925	11.3110	11.3110	0.0000			1335	11.9624	11.9625	-0.0001			
930	11.3201	11.3202	-0.0001			1340	11.9695	11.9696	-0.0001			
935	11.3291	11.3293	-0.0002			1345	11.9765	11.9768	-0.0003			
940	11.3381	11.3385	-0.0004			1350	11.9836	11.9839	-0.0003			
945	11.3470	11.3476	-0.0006			1355	11.9906	11.9910	-0.0004			
950	11.3558	11.3567	-0.0009			1360	11.9976	11.9980	-0.0004			
950.864911	11.3583	955	11.3646	11.3654	-0.0008			1365	12.0046	12.0051	-0.0005	
5420.163089	11.3583	960	11.3734	11.3739	-0.0005			1370	12.0116	12.0121	-0.0005	
17	3.48245516 3.80663410	965	11.3820	11.3824	-0.0004			1375	12.0185	12.0191	-0.0006	
		970	11.3907	11.3909	-0.0002			1380	12.0255	12.0261	-0.0006	
		975	11.3993	11.3994	-0.0001			1385	12.0324	12.0331	-0.0007	
		980	11.4079	11.4079	0.0000			1390	12.0393	12.0401	-0.0008	
		985	11.4164	11.4163	0.0001			1395	12.0462	12.0470	-0.0008	
		990	11.4249	11.4247	0.0002			1400	12.0531	12.0539	-0.0008	
		995	11.4333	11.4331	0.0002			1405	12.0599	12.0608	-0.0009	
		1000	11.4418	11.4415	0.0003			1410	12.0668	12.0677	-0.0009	
		1005	11.4502	11.4499	0.0003			1415	12.0736	12.0746	-0.0010	
		1010	11.4585	11.4582	0.0003			1420	12.0805	12.0814	-0.0009	
		1015	11.4668	11.4666	0.0002			1425	12.0873	12.0882	-0.0009	
		1020	11.4751	11.4749	0.0002			1430	12.0941	12.0950	-0.0009	
		1025	11.4834	11.4832	0.0002			1435	12.1009	12.1018	-0.0009	
		1030	11.4917	11.4915	0.0002			1440	12.1077	12.1086	-0.0009	
		1035	11.4999	11.4998	0.0001			1445	12.1145	12.1153	-0.0008	
		1040	11.5081	11.5080	0.0001			1450	12.1213	12.1221	-0.0008	
		1045	11.5163	11.5162	0.0001			1455	12.1281	12.1288	-0.0007	
		1050	11.5244	11.5245	-0.0001			1460	12.1349	12.1354	-0.0005	
		1055	11.5326	11.5326	0.0000			1465	12.1417	12.1421	-0.0004	
		1060	11.5407	11.5408	-0.0001			1470	12.1485	12.1488	-0.0003	
		1065	11.5488	11.5490	-0.0002			1475	12.1553	12.1554	-0.0001	
		1070	11.5569	11.5571	-0.0002			1480	12.1620	12.1620	0.0000	
		1075	11.5649	11.5652	-0.0003			1485	12.1688	12.1686	0.0002	
1080	11.5730	11.5734	-0.0004			1490	12.1755	12.1752	0.0003			
1085	11.5810	11.5814	-0.0004			1495	12.1822	12.1817	0.0005			
1090	11.5890	11.5895	-0.0005			1500	12.1889	12.1882	0.0007			
1095	11.5970	11.5976	-0.0006			1505	12.1956	12.1948	0.0008			
1100	11.6049	11.6056	-0.0007			1510	12.2023	12.2013	0.0010			
1105	11.6129	11.6136	-0.0007			1515	12.2089	12.2077	0.0012			
1110	11.6208	11.6216	-0.0008									

**Table 3**

Data MZY		Depth (km)	P-wave velocity (km/s)			Data MZY		p. 3/4	P-wave velocity (km/s)					
Radius (km)	$V_i$ (km/s)		Radius of surface-focus = 6371.028			Radius (km)	$V_i$ (km/s)		Depth (km)	Herrin & al.	MZY	Residual		
Layers	$B_i$ ( $\times 10^{-2}$ )		Herrin & al.	MZY	Residual	Layers	$B_i$ ( $\times 10^{-2}$ )							
4854.070549	12.2103	1520	12.2155	12.2142	0.0013	4526.927109	12.5946	1845	12.5982	12.5957	0.0025			
18	3.49547729 3.82197670	1525	12.2221	12.2207	0.0014	19	3.65834366 4.01545527	1850	12.6037	12.6018	0.0019			
		1530	12.2287	12.2272	0.0015			1855	12.6093	12.6079	0.0014			
		1535	12.2352	12.2337	0.0015			1860	12.6149	12.6141	0.0008			
		1540	12.2417	12.2402	0.0015			1865	12.6205	12.6201	0.0004			
		1545	12.2482	12.2466	0.0016			1870	12.6262	12.6262	0.0000			
		1550	12.2547	12.2530	0.0017			1875	12.6319	12.6322	-0.0003			
		1555	12.2611	12.2594	0.0017			1880	12.6376	12.6383	-0.0007			
		1560	12.2675	12.2658	0.0017			1885	12.6433	12.6443	-0.0010			
		1565	12.2738	12.2721	0.0017			1890	12.6491	12.6502	-0.0011			
		1570	12.2801	12.2784	0.0017			1895	12.6549	12.6562	-0.0013			
		1575	12.2864	12.2848	0.0016			1900	12.6607	12.6621	-0.0014			
		1580	12.2926	12.2910	0.0016			1905	12.6666	12.6680	-0.0014			
		1585	12.2988	12.2973	0.0015			1910	12.6725	12.6739	-0.0014			
		1590	12.3050	12.3036	0.0014			1915	12.6784	12.6798	-0.0014			
		1595	12.3111	12.3098	0.0013			1920	12.6843	12.6856	-0.0013			
		1600	12.3172	12.3160	0.0012			1925	12.6902	12.6914	-0.0012			
		1605	12.3232	12.3222	0.0010			1930	12.6962	12.6972	-0.0010			
		1610	12.3292	12.3284	0.0008			1935	12.7022	12.7030	-0.0008			
		1615	12.3352	12.3345	0.0007			1940	12.7082	12.7087	-0.0005			
		1620	12.3411	12.3407	0.0004			1945	12.7142	12.7144	-0.0002			
		1625	12.3471	12.3468	0.0003			1950	12.7202	12.7202	0.0000			
		1630	12.3530	12.3529	0.0001			1955	12.7262	12.7258	0.0004			
		1635	12.3589	12.3589	0.0000			1960	12.7323	12.7315	0.0008			
		1640	12.3648	12.3650	-0.0002			1965	12.7383	12.7371	0.0012			
		1645	12.3706	12.3710	-0.0004			1970	12.7444	12.7427	0.0017			
		1650	12.3765	12.3770	-0.0005			1975	12.7505	12.7483	0.0022			
		1655	12.3823	12.3830	-0.0007			1980	12.7565	12.7539	0.0026			
		1660	12.3882	12.3890	-0.0008			1981.009473	12.7550	20	1985	12.7626	12.7601	0.0025
		1665	12.3940	12.3950	-0.0010			4390.018527	12.7550		1990	12.7687	12.7664	0.0023
		1670	12.3999	12.4009	-0.0010			20	3.78936074 4.17166810		1995	12.7747	12.7726	0.0021
		1675	12.4057	12.4068	-0.0011						2000	12.7808	12.7789	0.0019
		1680	12.4115	12.4127	-0.0012						2005	12.7868	12.7851	0.0017
		1685	12.4173	12.4186	-0.0013						2010	12.7928	12.7913	0.0015
		1690	12.4231	12.4244	-0.0013						2015	12.7988	12.7975	0.0013
		1695	12.4289	12.4302	-0.0013						2020	12.8048	12.8037	0.0011
		1700	12.4347	12.4360	-0.0013						2025	12.8108	12.8098	0.0010
1705	12.4405	12.4418	-0.0013	2030	12.8167	12.8159	0.0008							
1710	12.4463	12.4476	-0.0013	2035	12.8227	12.8220	0.0007							
1715	12.4521	12.4533	-0.0012	2040	12.8286	12.8280	0.0006							
1720	12.4578	12.4591	-0.0013	2045	12.8345	12.8341	0.0004							
1725	12.4636	12.4648	-0.0012	2050	12.8403	12.8401	0.0002							
1730	12.4693	12.4705	-0.0012	2055	12.8462	12.8461	0.0001							
1735	12.4751	12.4761	-0.0010	2060	12.8520	12.8520	0.0000							
1740	12.4808	12.4818	-0.0010	2065	12.8578	12.8580	-0.0002							
1745	12.4865	12.4874	-0.0009	2070	12.8636	12.8639	-0.0003							
1750	12.4922	12.4930	-0.0008	2075	12.8693	12.8698	-0.0005							
1755	12.4978	12.4986	-0.0008	2080	12.8751	12.8757	-0.0006							
1760	12.5035	12.5041	-0.0006	2085	12.8808	12.8815	-0.0007							
1765	12.5091	12.5097	-0.0006	2090	12.8865	12.8873	-0.0008							
1770	12.5148	12.5152	-0.0004	2095	12.8922	12.8931	-0.0009							
1775	12.5204	12.5207	-0.0003	2100	12.8979	12.8989	-0.0010							
1780	12.5259	12.5262	-0.0003	2105	12.9036	12.9046	-0.0010							
1785	12.5315	12.5316	-0.0001	2110	12.9092	12.9104	-0.0012							
1790	12.5371	12.5371	0.0000	2115	12.9149	12.9161	-0.0012							
1795	12.5426	12.5425	0.0001	2120	12.9205	12.9217	-0.0012							
1800	12.5481	12.5479	0.0002	2125	12.9262	12.9274	-0.0012							
1805	12.5537	12.5533	0.0004	2130	12.9318	12.9330	-0.0012							
1810	12.5592	12.5586	0.0006	2135	12.9375	12.9386	-0.0011							
1815	12.5648	12.5639	0.0009	2140	12.9431	12.9442	-0.0011							
1820	12.5703	12.5693	0.0010	2145	12.9487	12.9497	-0.0010							
1825	12.5759	12.5745	0.0014	2150	12.9544	12.9552	-0.0008							
1830	12.5814	12.5798	0.0016	2155	12.9601	12.9607	-0.0006							
1835	12.5870	12.5851	0.0019	2160	12.9657	12.9662	-0.0005							
1844.100891	12.5946	1840	12.5926	12.5903	0.0023	2165	12.9714			12.9717	-0.0003			
2201.417284	13.0106					2170	12.9771			12.9771	0.0000			
						2175	12.9829	12.9825	0.0004					
						2180	12.9886	12.9879	0.0007					
						2185	12.9944	12.9932	0.0012					
						2190	13.0002	12.9985	0.0017					
						2195	13.0059	13.0038	0.0021					
2200	13.0117	13.0091	0.0026											



**Table 3**

Data MZY		Depth (km)	P-wave velocity (km/s)			Data MZY		p. 4/4	P-wave velocity (km/s)		
Radius (km)	$V_j$ (km/s)		Herrin & al.	MZY	Residual	Radius (km)	$V_j$ (km/s)		Herrin & al.	MZY	Residual
Layers $B_j$ ( $\times 10^{-2}$ )		Depth (km)	Radius of surface-focus = 6371.028			Layers $B_j$ ( $\times 10^{-2}$ )		Depth (km)	H. & al. - MZY		
Depth (km)			H. & al. - MZY			Layers $A_j$ ( $\times 10^{-3}$ )			H. & al. - MZY		
			H. & al. - MZY					H. & al. - MZY			
4169.610716	13.0106	2205	13.0175	13.0151	0.0024	3887.018610	13.3469	2485	13.3499	13.3482	0.0017
<b>21</b>	3.96471462 4.38203609	2210	13.0234	13.0214	0.0020	<b>23</b>	4.28150596 4.76460375	2490	13.3562	13.3549	0.0013
		2215	13.0292	13.0277	0.0015			2495	13.3626	13.3615	0.0011
		2220	13.0350	13.0339	0.0011			2500	13.3690	13.3680	0.0010
		2225	13.0408	13.0401	0.0007			2505	13.3753	13.3746	0.0007
		2230	13.0466	13.0462	0.0004			2510	13.3817	13.3811	0.0006
		2235	13.0525	13.0524	0.0001			2515	13.3881	13.3876	0.0005
		2240	13.0583	13.0585	-0.0002			2520	13.3945	13.3940	0.0005
		2245	13.0641	13.0646	-0.0005			2525	13.4009	13.4004	0.0005
		2250	13.0700	13.0707	-0.0007			2530	13.4073	13.4068	0.0005
		2255	13.0758	13.0767	-0.0009			2535	13.4137	13.4132	0.0005
		2260	13.0817	13.0827	-0.0010			2540	13.4200	13.4195	0.0005
		2265	13.0876	13.0887	-0.0011			2545	13.4264	13.4258	0.0006
		2270	13.0934	13.0947	-0.0013			2550	13.4327	13.4321	0.0006
		2275	13.0993	13.1006	-0.0013			2555	13.4391	13.4383	0.0008
		2280	13.1052	13.1065	-0.0013			2560	13.4454	13.4445	0.0009
		2285	13.1110	13.1124	-0.0014			2565	13.4516	13.4507	0.0009
		2290	13.1169	13.1182	-0.0013			2570	13.4578	13.4568	0.0010
		2295	13.1228	13.1241	-0.0013			2575	13.4640	13.4629	0.0011
		2300	13.1287	13.1298	-0.0011			2580	13.4702	13.4690	0.0012
		2305	13.1345	13.1356	-0.0011			2585	13.4763	13.4750	0.0013
2310	13.1404	13.1414	-0.0010	2590	13.4823	13.4810	0.0013				
2315	13.1462	13.1471	-0.0009	2595	13.4883	13.4870	0.0013				
2320	13.1521	13.1528	-0.0007	2600	13.4942	13.4930	0.0012				
2325	13.1579	13.1584	-0.0005	2605	13.5000	13.4989	0.0011				
2330	13.1637	13.1641	-0.0004	2610	13.5058	13.5048	0.0010				
2335	13.1696	13.1697	-0.0001	2615	13.5116	13.5106	0.0010				
2340	13.1754	13.1753	0.0001	2620	13.5172	13.5164	0.0008				
2345	13.1812	13.1808	0.0004	2625	13.5229	13.5222	0.0007				
2350	13.1871	13.1863	0.0008	2630	13.5285	13.5280	0.0005				
2355	13.1929	13.1918	0.0011	2635	13.5340	13.5337	0.0003				
2360	13.1987	13.1973	0.0014	2640	13.5394	13.5394	0.0000				
2365	13.2046	13.2028	0.0018	2645	13.5448	13.5451	-0.0003				
2370	13.2104	13.2082	0.0022	2650	13.5501	13.5507	-0.0006				
2375	13.2163	13.2141	0.0022	2655	13.5554	13.5563	-0.0009				
2380	13.2221	13.2205	0.0016	2660	13.5606	13.5619	-0.0013				
2385	13.2280	13.2268	0.0012	2665	13.5657	13.5666	-0.0009				
2390	13.2339	13.2332	0.0007	2670	13.5707	13.5712	-0.0005				
2395	13.2397	13.2395	0.0002	2675	13.5756	13.5758	-0.0002				
2400	13.2456	13.2458	-0.0002	2680	13.5804	13.5804	0.0000				
2405	13.2515	13.2520	-0.0004	2685	13.5851	13.5849	0.0002				
2410	13.2575	13.2582	-0.0007	2690	13.5898	13.5894	0.0004				
2415	13.2635	13.2644	-0.0009	2695	13.5942	13.5938	0.0004				
2420	13.2694	13.2706	-0.0012	2700	13.5986	13.5983	0.0003				
2425	13.2755	13.2767	-0.0012	2705	13.6027	13.6027	0.0000				
2430	13.2815	13.2828	-0.0013	2710	13.6067	13.6071	-0.0004				
2435	13.2876	13.2889	-0.0013	2715	13.6105	13.6106	-0.0001				
2440	13.2937	13.2950	-0.0013	2720	13.6140	13.6137	0.0003				
2445	13.2998	13.3010	-0.0012	2725	13.6173	13.6168	0.0005				
2450	13.3060	13.3070	-0.0010	2730	13.6205	13.6199	0.0006				
2455	13.3122	13.3129	-0.0007	2735	13.6234	13.6229	0.0005				
2460	13.3184	13.3188	-0.0004	2740	13.6261	13.6259	0.0002				
2465	13.3247	13.3247	0.0000	2745	13.6287	13.6289	-0.0002				
2470	13.3310	13.3306	0.0004	2750	13.6312	13.6318	-0.0006				
2475	13.3372	13.3365	0.0007	2755	13.6336	13.6335	0.0001				
2480	13.3436	13.3423	0.0013	2760	13.6359	13.6350	0.0009				
<b>22</b>	4.13594750 4.58849794	2375	13.2163	13.2141	0.0022	2765	13.6381	13.6366	0.0015		
		2380	13.2221	13.2205	0.0016	2770	13.6402	13.6382	0.0020		
		2385	13.2280	13.2268	0.0012	2775	13.6422	13.6397	0.0025		
		2390	13.2339	13.2332	0.0007	2780	13.6441	13.6411	0.0030		
		2395	13.2397	13.2395	0.0002	2785	13.6460	13.6409	0.0051		
		2400	13.2456	13.2458	-0.0002	2790	13.6478	13.6403	0.0075		
		2405	13.2515	13.2520	-0.0004	2795	13.6495	13.6397	0.0098		
		2410	13.2575	13.2582	-0.0007	2800	13.6512	13.6391	0.0121		
		2415	13.2635	13.2644	-0.0009	2805	13.6528	13.6332	0.0196		
		2420	13.2694	13.2706	-0.0012	2810	13.6544	13.6264	0.0280		
<b>23</b>	4.13634936 4.58799171	2425	13.2755	13.2767	-0.0012	2815	13.6559	13.6310	0.0249		
		2430	13.2815	13.2828	-0.0013	2820	13.6574	13.6358	0.0216		
		2435	13.2876	13.2889	-0.0013	2825	13.6588	13.6405	0.0183		
		2440	13.2937	13.2950	-0.0013	2830	13.6601	13.6452	0.0149		
		2445	13.2998	13.3010	-0.0012	2835	13.6613	13.6499	0.0114		
		2450	13.3060	13.3070	-0.0010	2840	13.6625	13.6545	0.0080		
		2455	13.3122	13.3129	-0.0007	2845	13.6636	13.6592	0.0044		
		2460	13.3184	13.3188	-0.0004	2850	13.6646	13.6637	0.0009		
		2465	13.3247	13.3247	0.0000	2855	13.6655	13.6683	-0.0028		
		2470	13.3310	13.3306	0.0004	2860	13.6663	13.6728	-0.0065		
<b>24</b>	4.13634936 4.58799171	2475	13.3372	13.3365	0.0007	2865	13.6670	13.6772	-0.0102		
		2480	13.3436	13.3423	0.0013	2870	13.6677	13.6817	-0.0140		
		2485	13.3499	13.3482	0.0017	2875	13.6683	13.6861	-0.0178		
		2490	13.3562	13.3549	0.0013	2880	13.6689	13.6904	-0.0215		
		2495	13.3626	13.3615	0.0011	2885	13.6694	13.6948	-0.0254		
		2500	13.3690	13.3680	0.0010	2890	13.6698	13.6991	-0.0293		
		2505	13.3753	13.3746	0.0007	2895	13.6700				
		2510	13.3817	13.3811	0.0006						
		2515	13.3881	13.3876	0.0005						
		2520	13.3945	13.3940	0.0005						
2525	13.4009	13.4004	0.0005								
2530	13.4073	13.4068	0.0005								
2535	13.4137	13.4132	0.0005								
2540	13.4200	13.4195	0.0005								
2545	13.4264	13.4258	0.0006								
2550	13.4327	13.4321	0.0006								
2555	13.4391	13.4383	0.0008								
2560	13.4454	13.4445	0.0009								
2565	13.4516	13.4507	0.0009								
2570	13.4578	13.4568	0.0010								
2575	13.4640	13.4629	0.0011								
2580	13.4702	13.4690	0.0012								
2585	13.4763	13.4750	0.0013								
2590	13.4823	13.4810	0.0013								
2595	13.4883	13.4870	0.0013								
2600	13.4942	13.4930	0.0012								
2605	13.5000	13.4989	0.0011								
2610	13.5058	13.5048	0.0010								
2615	13.5116	13.5106	0.0010								
2620	13.5172	13.5164	0.0008								
2625	13.5229	13.5222	0.0007								
2630	13.5285	13.5280	0.0005								
2635	13.5340	13.5337	0.0003								
2640	13.5394	13.5394	0.0000								
2645	13.5448	13.5451	-0.0003								
2650	13.5501	13.5507	-0.0006								
2655	13.5554	13.5563	-0.0009								
2660	13.5606	13.5619	-0.0013								
2665	13.5657	13.5666	-0.0009								
2670	13.5707	13.5712	-0.0005								
2675	13.5756	13.5758	-0.0002								
2680	13.5804	13.5804	0.0000								
2685	13.5851	13.5849	0.0002								
2690	13.5898	13.5894	0.0004								
2695	13.5942	13.5938	0.0004								
2700	13.5986	13.5983	0.0003								
2705	13.6027	13.6027	0.0000								

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